

### Problem Set 3

#### Problem 2

$$\left(\frac{\partial f}{\partial x}\right)_y = 5xy \cos 5x + y \sin 5x - 12xe^{-2x^2} \cos y + 2x\sqrt{y} \ln y$$

$$\left(\frac{\partial f}{\partial y}\right)_x = x \sin 5x + \frac{x^2}{\sqrt{y}} + \frac{x^2 \ln y}{2\sqrt{y}} - 3e^{-2x^2} \sin y$$

$$\left(\frac{\partial^2 f}{\partial x^2}\right)_y = 10y \cos 5x - 25xy \sin 5x - 12e^{-2x^2} \cos y + 48e^{-2x^2} x^2 \cos y + 2\sqrt{y} \ln y$$

$$\left(\frac{\partial^2 f}{\partial y^2}\right)_x = -3e^{-2x^2} \cos y - \frac{x^2 \ln y}{4y^{\frac{3}{2}}}$$

$$\left(\frac{\partial}{\partial x}\left(\frac{\partial f}{\partial y}\right)_y\right)_y = \frac{2x}{\sqrt{y}} + \frac{x \ln y}{\sqrt{y}} + \sin 5x + 5x \cos 5x + 12e^{-2x^2} x \sin y$$

$$\left(\frac{\partial}{\partial y}\left(\frac{\partial f}{\partial x}\right)_x\right)_x = 5x \cos 5x + 12e^{-2x^2} x \sin y + \frac{2x}{\sqrt{y}} + \frac{x \ln y}{\sqrt{y}} + \sin 5x = \left(\frac{\partial}{\partial x}\left(\frac{\partial f}{\partial y}\right)_x\right)_y$$

$$df = \left(\frac{\partial f}{\partial x}\right)_y dx + \left(\frac{\partial f}{\partial y}\right)_x dy = (5xy \cos 5x + y \sin 5x - 12xe^{-2x^2} \cos y + 2x\sqrt{y} \ln y) dx + \left(x \sin 5x + \frac{x^2}{\sqrt{y}} + \frac{x^2 \ln y}{2\sqrt{y}} - 3e^{-2x^2} \sin y\right) dy$$

#### Problem 4

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_p = \frac{\rho}{m} \left(\frac{\partial \frac{m}{\rho}}{\partial T}\right)_p = \frac{\rho}{m} \left(\frac{\partial \frac{m}{\rho}}{\partial \rho}\right)_p \left(\frac{\partial \rho}{\partial T}\right)_p = \frac{\rho}{m} \left(-\frac{m}{\rho^2}\right) \left(\frac{\partial \rho}{\partial T}\right)_p = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T}\right)_p$$

#### Problem 5

$$\begin{aligned} \Delta P &= \int \frac{\beta_{\text{water}}}{\kappa} dT - \int \frac{1}{\kappa V} dV \approx \frac{\beta_{\text{water}}}{\kappa} \Delta T - \frac{1}{\kappa} \ln \frac{V_f}{V_i} \\ &= \frac{\beta_{\text{water}}}{\kappa} \Delta T - \frac{1}{\kappa} \ln \frac{V_i (1 + \beta_{\text{vessel}} \Delta T)}{V_i} \approx \frac{\beta_{\text{water}}}{\kappa} \Delta T - \frac{1}{\kappa} \frac{V_i \beta_{\text{vessel}} \Delta T}{V_i} = \frac{(\beta_{\text{water}} - \beta_{\text{vessel}})}{\kappa} \Delta T \\ &= \frac{(2.07 - 1.02) \times 10^{-4} (\text{°C})^{-1}}{4.59 \times 10^{-5} (\text{bar})^{-1}} \times 60.0 \text{°C} = 77.8 \text{ bar} \end{aligned}$$

$$P_i + \Delta P = 78.8 \text{ bar}$$

**Problem 9**

$$\frac{C_{P,m}}{R} = 3.093 + 6.967 \times 10^{-3} \frac{T}{\text{K}} - 45.81 \times 10^{-7} \frac{T^2}{\text{K}^2} + 1.035 \times 10^{-9} \frac{T^3}{\text{K}^3}. \text{ In this equation, } T \text{ is}$$

the absolute temperature in Kelvin. The ratios  $\frac{T^n}{\text{K}^n}$  ensure that  $C_{P,m}$  has the correct

dimension. Assuming ideal gas behavior, calculate  $q$ ,  $w$ ,  $\Delta U$ , and  $\Delta H$  if 1 mol of  $\text{SO}_2(\text{g})$  is heated from  $75^\circ$  to  $1350^\circ\text{C}$  at a constant pressure of 1 bar. Explain the sign of  $w$ .

$$\begin{aligned} \Delta H = q &= n \int_{T_i}^{T_f} C_{P,m} dT = 8.314 \text{ J mol}^{-1} \text{K}^{-1} \times \int_{348.15}^{1623.15} \left( 3.093 + 6.967 \times 10^{-3} \frac{T}{\text{K}} - 45.81 \times 10^{-7} \frac{T^2}{\text{K}^2} + 1.035 \times 10^{-9} \frac{T^3}{\text{K}^3} \right) d \frac{T}{\text{K}} \\ &= 1 \text{ mol} \times 8.314 \text{ J mol}^{-1} \times \left[ 3.093 \frac{T}{\text{K}} + 0.0034835 \frac{T^2}{\text{K}^2} - 1.527 \times 10^{-6} \frac{T^3}{\text{K}^3} + 2.5875 \times 10^{-10} \frac{T^4}{\text{K}^4} \right]_{348.15}^{1623.15} \\ &= \left( 1 \text{ mol} \times 3.279 \times 10^4 \text{ J mol}^{-1} + 7.279 \times 10^4 \text{ J mol}^{-1} - 5.375 \times 10^4 \text{ J mol}^{-1} + 1.490 \times 10^4 \text{ J mol}^{-1} \text{K}^{-1} \right) \\ &= 6.67 \times 10^4 \text{ J} \end{aligned}$$

$$\begin{aligned} \Delta U &= \Delta H - \Delta(PV) = \Delta H - nR\Delta T \\ &= 6.673 \times 10^4 \text{ J} - 1 \text{ mol} \times 8.314 \text{ J mol}^{-1} \text{K}^{-1} \times (1623.15 \text{ K} - 348.15 \text{ K}) \\ &= 5.61 \times 10^4 \text{ J} \\ w &= \Delta U - q = 5.613 \times 10^4 \text{ J} - 6.673 \times 10^4 \text{ J} = -1.06 \times 10^4 \text{ J} \end{aligned}$$

**Problem 13**

$$\begin{aligned} \beta &= \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P = \frac{1}{V} \frac{nR}{P}; \quad \kappa = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T = \frac{nRT}{VP^2} = \frac{1}{P} \\ C_p - C_v &= TV \frac{\beta^2}{\kappa} = TV \left( \frac{1}{V} \frac{nR}{P} \right)^2 P = TV \frac{n^2 R^2}{V^2 P} = nR \end{aligned}$$

**Problem 19**

$$\begin{aligned} \Delta H_m &= - \int_{P_i}^{P_f} C_{P,m} \mu_{J,T} dP \approx -C_{P,m} \mu_{J,T} (P_f - P_i) \\ &= -C_{P,m} \times \frac{1}{C_{P,m}} \left( \frac{2 \times 0.1355 \text{ m}^6 \text{ Pa mol}^{-2}}{8.314 \text{ J mol}^{-1} \text{K}^{-1} \times 300 \text{ K}} - 0.03201 \times 10^{-3} \text{ m}^3 \text{ mol}^{-1} \right) \times (1.00 \times 10^5 \text{ Pa} - 400 \times 10^5 \text{ Pa}) \\ &= 3.06 \times 10^3 \text{ J} \end{aligned}$$

For an ideal gas,  $\Delta H_m = 0$  because  $\mu_{J,T}$  is zero for an ideal gas.

**Problem 22**

$$\left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial P}{\partial T}\right)_V - P = -T \left(\frac{\partial V}{\partial T}\right)_P - P = T \frac{V\beta}{V\kappa} - P = T \frac{\beta}{\kappa} - P$$

**Problem 23**

The internal pressure of a gas is given by

$$\left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial P}{\partial T}\right)_V - P$$

Using the Redlich-Kwong equation of state,

$$\begin{aligned} \left(\frac{\partial P}{\partial T}\right)_V &= \frac{R}{V_m - b} + \frac{1}{2} \frac{a}{T^{3/2} V_m (V_m + b)} \\ \left(\frac{\partial U}{\partial V}\right)_T &= T \left(\frac{\partial P}{\partial T}\right)_V - P = \frac{RT}{V_m - b} + \frac{1}{2} \frac{a}{\sqrt{T} V_m (V_m + b)} - \left( \frac{RT}{V_m - b} - \frac{a}{\sqrt{T} V_m (V_m + b)} \right) \\ &= \frac{1}{2} \frac{a}{\sqrt{T} V_m (V_m + b)} + \frac{a}{\sqrt{T} V_m (V_m + b)} = \frac{3a}{2\sqrt{T} V_m (V_m + b)} \end{aligned}$$

**Problem 26**

$$\left(\frac{\partial C_V}{\partial V}\right)_T = \left(\frac{\partial}{\partial V} \left(\frac{\partial U}{\partial T}\right)_V\right)_T = \left(\frac{\partial}{\partial T} \left(\frac{\partial U}{\partial V}\right)_T\right)_T$$

The order of differentiation can be reversed because  $U$  is a state function.

$$\text{Using the equation } \left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial P}{\partial T}\right)_V - P$$

$$\begin{aligned} \left(\frac{\partial C_V}{\partial V}\right)_T &= \left(\frac{\partial}{\partial T} \left( T \left(\frac{\partial P}{\partial T}\right)_V - P \right)\right)_V \\ &= \left(\frac{\partial P}{\partial T}\right)_V + T \left(\frac{\partial^2 P}{\partial T^2}\right)_V - \left(\frac{\partial P}{\partial T}\right)_V = T \left(\frac{\partial^2 P}{\partial T^2}\right)_V \end{aligned}$$

**Problem 29**

$$\left( \frac{\partial}{\partial T} \left( \frac{\partial H}{\partial P} \right) \right)_T = \left( \frac{\partial}{\partial P} \left( \frac{\partial H}{\partial T} \right) \right)_T = \left( \frac{\partial C_{P,m}}{\partial P} \right)_T$$

Equation 3.44 states that

$$\left( \frac{\partial H}{\partial P} \right)_T = V - T \left( \frac{\partial V}{\partial T} \right)_P$$

Therefore,

$$\begin{aligned} \left( \frac{\partial C_{P,m}}{\partial P} \right)_T &= \left( \frac{\partial}{\partial T} \left( V - T \left( \frac{\partial V}{\partial T} \right)_P \right) \right)_P \\ &= \left( \frac{\partial}{\partial T} \left( (RT/P) + B(T) - T \left( \frac{\partial [(RT/P) + B(T)]}{\partial T} \right)_P \right) \right)_P \\ &= \left( \frac{\partial}{\partial T} \left( (RT/P) + B(T) - T \left( \frac{R}{P} + \frac{dB(T)}{dT} \right)_P \right) \right)_P \\ &= \left( \frac{R}{P} + \frac{dB(T)}{dT} - \frac{R}{P} - \frac{dB(T)}{dT} + T \frac{d^2B(T)}{dT^2} \right)_P \\ &= T \frac{d^2B(T)}{dT^2} \end{aligned}$$